

## New approaches to modelling heat/mass transfer processes in spherical and non-spherical mono-component droplets

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### Introduction

The importance of accurately modelling the heating and evaporation of spherical and non-spherical droplets is well known and has been described in numerous papers and books summarised in the monographs [4, 5]. These processes have many industrial applications, including spray drying and combustion, some of which are discussed in [4, 5]. This abstract is focused on a brief analysis of new approaches to modelling heat/mass transfer processes in spherical and non-spherical mono-component droplets, obtained after the publication of [4, 5].

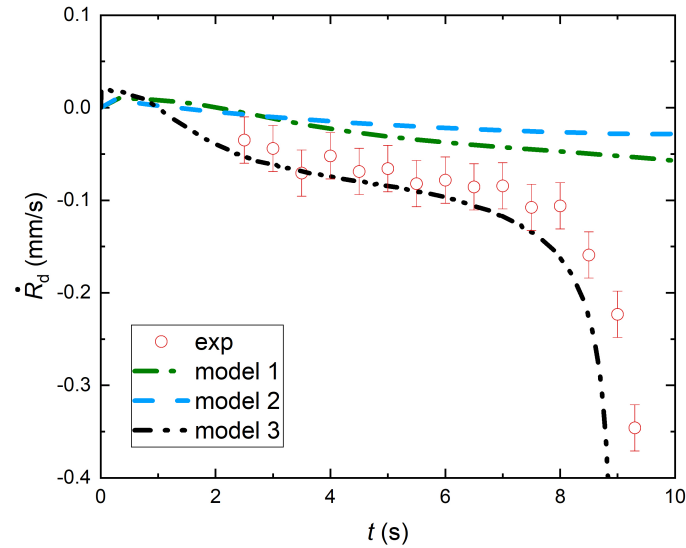
### Material and methods

The abstract is focused on the analysis of spherical and spheroidal droplets heated in ambient gas (air), based on a combination of analytical and numerical methods. The analytical solutions of heat and mass transfer equations in the gas and liquid phases were obtained, if possible. Then these solutions in the gas phase were used as boundary conditions for the liquid phase. Thus the new analytical-numerical method was developed and applied to a specific problem of droplet heating and evaporation. In this method the predictions of the analytical or numerical solutions at the end of each time step are used as initial conditions for the following time steps with updated values of input parameters

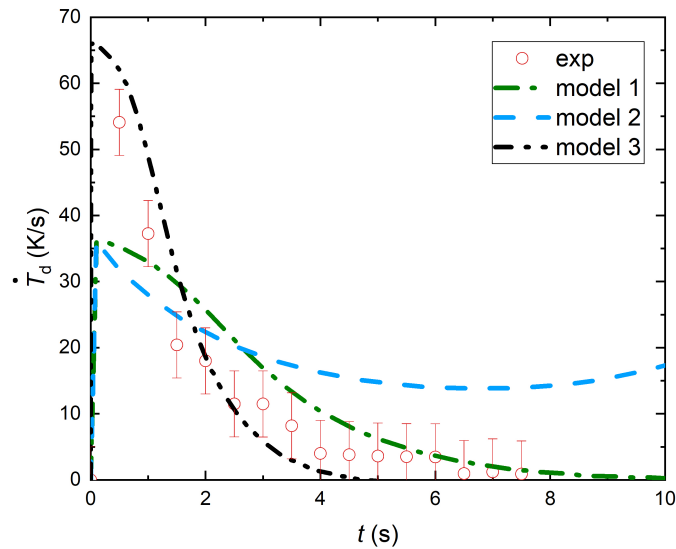
### Results and Discussion

Recent developments in the modelling of heating and evaporation of spherical and non-spherical mono-component droplets ([6, 2, 1, 3]) are reviewed. These include the model linking the previously developed liquid phase model, using the analytical solution to the heat transfer equation at each time step, and the gas phase model, using the solution to the equations of the conservation of mass, momentum, and energy leading to an explicit expression for the Nusselt number and implicit expression for evaporation rate of the droplet [2] (called Model 3). The predictions of the numerical algorithms for this and the previously developed approaches are compared with experimentally observed time dependencies of the rates of change of radii and average temperatures of n-decane droplets at initial temperatures and radii equal to 300 K and 0.85 mm, respectively, placed in a gas at temperature 760 K. The results of the comparison are shown in Figure 1. In Model 1, to which Figure 1 refers, the heat rate, supplied to the droplets to raise their internal energy, is calculated based on the observation that steady-state equations for heat and mass balance in the gas phase should lead to the same droplet evaporation rates. The direct calculation of the above-mentioned heat rate is used in Model 2; the value of this rate is then used for the estimation of the droplet evaporation rate using the Spalding heat transfer number [1].

It can be seen from Figure 1 that the experimentally observed  $\dot{R}_d$  and  $\dot{T}_d$  are reasonably close to those predicted by Model 3. The deviations between the observed values of  $\dot{R}_d$  and  $\dot{T}_d$



(a)



(b)

**Figure 1.** Plots of rate of change of radius ( $\dot{R}_d$ ) and average temperature ( $\dot{T}_d$ ) of an n-decane droplet versus time predicted by Models 1, 2 and 3 and observed experimentally (exp). Gas temperature  $T_g$  was  $760 \pm 10$  K; initial droplet temperature ( $T_{d0}$ ) and radius ( $R_{d0}$ ) were  $300 \pm 10$  K and  $0.85 \pm 0.05$  mm, respectively. Copyright Elsevier (2024)

and those predicted by Models 1 and 2 are quite large. These models even predict different trends of change for these parameters, which limits their suitability for studying the time evolution of these parameters during droplet heating/evaporation. The trends similar to those illustrated in Figure 1 were also shown for the ambient gas temperature equal to  $500 \pm 10$  K. A mathematical model for spheroidal droplet heating and evaporation takes into account the effect of liquid finite thermal conductivity and is based on the previously obtained analytical solution for the vapour mass fraction at the droplet surface and a new correlation for the convective heat transfer coefficient incorporated into the numerical code. The heat transfer equation in the liquid phase is solved numerically using the finite element heat transfer module of COMSOL Multiphysics [3].

It is shown that the lifetimes of prolate and oblate droplets is shorter than that of spherical droplets of the same volume. The difference in these lifetimes is shown to increase with increasing aspect ratios for prolate droplets and decreasing aspect ratios for oblate droplets. The predictions of the model are shown to agree with experimental data. The maximal surface tem-

peratures are predicted near the areas with the maximal surface curvatures. The aspect ratios were shown to be weakly dependent on time, which is consistent with experimental data.

### Conclusion

A recently developed model of heating and evaporation of spherical droplets is described. This model links the previously developed liquid phase model, using the analytical solution to the heat transfer equation at each time step, and the gas phase model, based on the solution to the equations of the conservation of mass, momentum, and energy which leads to an explicit formula for the Nusselt number and a relatively simple equation for the evaporation rate of the droplet. It is shown that this model predicts the results closer to experimental data than the previously developed models.

A recently developed model for spheroidal droplet heating and evaporation is described. This model considered the effect of liquid finite thermal conductivity and is based on the analytical solution for the vapour mass fraction at the droplet surface and a correlation for the convective heat transfer coefficient. Both were incorporated into the numerical code.

### Nomenclature

$R$	droplet radius [m]
$t$	time [s]
$T$	temperature [T]

### Subscripts

d	droplet
g	ambient gas
0	initial

### Acknowledgments

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