

1 **AN EMPATHETIC ADDED SUSTAINABILITY INDEX (EASI) FOR**
2 **CEMENTITIOUS BASED CONSTRUCTION MATERIALS**

3 *Coppola^{1,2} L, Coffetti^{1,2} D, Crotti^{1,2} E, Gazzaniga G³, Pastore T^{1,2}.*

4 ¹ Department of Engineering and Applied Sciences, University of Bergamo (Italy)

5 ² Consorzio INSTM, UdR “Materials and Corrosion”, Florence (Italy)

6 ³ Department of Architecture, Built environment and Construction engineering, Politecnico di
7 Milano (Italy)

8 *luigi.coppola@unibg.it - denny.coffetti@unibg.it - elena.crotti@unibg.it -*

9 *gabriele.gazzaniga@polimi.it - tommaso.pastore@unibg.it*

10 **ABSTRACT**

11 The concrete industry is the largest consumer of natural resources and the Portland cement, the binder
12 of modern concrete mixtures, is not environmentally friendly. The world's cement production, in fact,
13 contributes to the earth's atmosphere about 5-7% of the total CO₂ emissions, CO₂ being mainly
14 responsible for global warming and climate change. As a consequence, concrete industry in the future
15 has to feed the growing population needs – expected to rise up to ten billion in 2050 - being
16 sustainable by means of the “3R-Green Strategy”: Reduction in consumption of gross energy,
17 Reduction in polluting emissions and Reduction in consuming not renewable natural resources. At
18 the same time, the concept of sustainable development in the concrete industry is not well defined
19 and, currently, there are no holistic models capable of assessing the environmental footprint of
20 cement-based materials. For this reason, a new Empathetic Added Sustainability Index (EASI) was
21 developed taking into account both the environmental impact of mortars and concretes through the
22 global warming potential (GWP), the gross energy requirement (GER) and the natural raw materials
23 consumption (NRMC) but also the durability performance and the engineering performance (such as
24 compressive and tensile strength, bond to reinforcing steel, shrinkage and creep, shear properties, etc)
25 required as a function of the specific application. EASI demonstrated that Alkali Activated Slag

26 (AAS) and High Volume Fly Ash (HVFA) reinforced concretes are characterized by the lower
27 environmental impact in chloride-rich environments. On the other hand, in CO₂-rich environments,
28 the best solution in terms of sustainability is represented by the HVFA concretes. Finally, for a
29 thermal plaster exposed to freeze and thaw cycles, EASI clearly showed that AAS lightweight plaster
30 is the most appropriate solution.

31 **KEYWORDS**

32 Sustainability; 3-R Strategy; Alternative Binders; Waste Management; Sustainability index.

33 **1. INTRODUCTION**

34 With a production of more than 10 billion cubic meters, concrete is the most widely used construction
35 material in the world, especially in areas with high economic and demographic growth, such as China
36 and India. Due to these huge volumes, the concrete industry – and in particular the cement sector –
37 has a very strong environmental impact in terms of greenhouse gas (GHG) emissions, energy
38 requirement and consumption of natural resources. In fact, it has been reported that cement
39 manufacturing is responsible for 5-7% of anthropogenic CO₂ emissions (Barcelo et al., 2014;
40 Maddalena et al., 2018; Salas et al., 2016), including the CO₂ released in the clinker industrial process
41 (CO₂: 520 kg CO₂/t of clinker) and by fuel combustion related to the energy use in clinker production
42 (CO₂: 350 kg CO₂/t of clinker). On average, 1.53 ton of raw materials (1.22 ton of limestone, 0.31
43 ton of clay) are required to produce 1 ton of ordinary Portland cement (Chen et al., 2010). Thus, the
44 cement and concrete industry is under pressure to reduce greenhouse gas emissions as well as both
45 energy and natural resources consumption (J. S. Damtoft et al., 2008), in other words, to be
46 sustainable. The task is particularly complicated since population is expected to reach ten billion in
47 2050. As a consequence of this, the main challenge for the concrete industry is how to support the
48 increasing demand of buildings and infrastructures of the growing population being at the same time

49 sustainable. The answer to this hard task is represented by the “**3R-Green Strategy**”: **Reduce energy**
50 **– Reduce pollutant emissions – Reduce consumption of natural resources.**

51 **2. THE “3-R GREEN STRATEGY”**

52 The first two steps of the virtuous path of “**3R-Green Strategy**” are represented by a strong effort in
53 reducing energy consumption and GHG emissions by means of the following items.

54 **2.1 The optimization of cement plants**

55 The optimization of cement plants can be obtained through a process of revision of fuels used.
56 However, switching from conventional to alternative fuels presents several challenges related to
57 higher SO₂, NO_x, and CO emissions (Gartner and Hirao, 2015; Puertas et al., 2008). For instance, in
58 mid 80s, tyres became very popular as alternative fuel to cope with the increasing fossil fuel costs.
59 However, CO, SO₂ and NO_x emissions increase while replacing Tyre Derived Fuel (TDF) up to 20%
60 of fossil fuel. Moreover, the availability of Municipal Solid Wastes (MSW) makes them one of the
61 most desirable alternative fuels in cement manufacturing. Unfortunately, during incineration of MSW
62 toxins and heavy metals are produced and partially transferred to the clinker (Pan et al., 2008).

63 Plastic wastes are potential candidates for alternative fuel in cement industry due to their worldwide
64 production and high calorific value 29-40 MJ/kg. However, if the chlorine content of plastic waste
65 exceeds 0.7% then it may impact on the quality of the clinker (Aranda Usón et al., 2013; Rahman et
66 al., 2015).

67 In conclusion, on the basis of the above mentioned items use of alternative fuels seems to be
68 ineffective in solving environmental problems related to clinker production.

69 **2.2 The limitation of the clinker factor**

70 It is possible to limit the clinker factor in cements by blending low-carbon supplementary
71 cementitious materials (SCMs), such as fly ash (FA) (Coppola et al., 2018a; Messina et al., 2018;
72 Van den Heede, P.; De Belie, 2010), ground granulated blast furnace slag (GGBFS) (Özbay et al.,
73 2016), metakaolin (MK) (Mobili et al., 2016) and natural pozzolans (Burak Uzal, P. Kumar Mehta,

74 n.d.). Moreover, SMCs can be used directly in ready-mix concrete plants to manufacture cementitious
75 mixtures where a slow strength gain is required.

76 In 2015, about 1000 million tons of fly-ash were generated in the world. However, only about 430
77 million tons of fly-ash were consumed in different applications including cement and concrete
78 industry (Fig. 1). Total fly ash production is forecasted to increase about 50% over the next fifteen
79 years (about 1500 million tons of fly-ash available in 2030) (*Global Fly Ash Market 2024, 2016,*
80 n.d.), because coal use is estimated to rise over 60% to 2030. In addition to the increase in fly-ash,
81 cement production is also expected to be 4830 million tons in 2030. Assuming to recover all the fly
82 ash produced in cement and concrete industry, only about 4000 million tons of clinker will need to
83 be produced (Fig. 1). In other words, thanks to the total recycling of fly-ash both in cement plants
84 and in ready-mix concrete it could be possible to feed the demand of buildings and infrastructures in
85 2030 without increasing ordinary Portland cement production with respect to that recorded in 2015
86 (Zementwerke, 2014).

87 **2.3 The use of alkali-activated materials**

88 These materials are raw silico-alumina materials (called precursors) mixed with huge amounts of
89 alkaline activators. In Alkali-Activated Materials (AAMs) the process of hardening is promoted by
90 the dissolution of silica favored by the alkaline activators which generally consist of sodium or
91 potassium silicate and/or hydroxide (Lamuta et al., 2016). Therefore, alkali-activated materials can
92 be considered “environmentally friendly” since it is not necessary (except for the metakaolin) to burn
93 materials used as precursors. One of the primary advantages of alkali activated slag (AAS) cements
94 relative to Portland cement from an environmental perspective is the lower greenhouse gases (GHG)
95 emissions and energy requirement (Tab. 1 – Fig. 2) (Duxson et al., 2007). Moreover, Coppola et al.
96 (Coppola et al., 2018d) showed the extreme versatility of mixture based on AAS cements (Fig. 3). In
97 general, a properly proportioned mixture makes possible to produce Portland cement-free mortars
98 and concretes with mechanical properties similar or higher than those of traditional OPC-based
99 mixtures, but with a reduction of GER (Gross Energy Requirement) and GWP (Global Warming

100 Potential) respectively about 70% - 80% and 80% - 90% compared to traditional mortars (Fig. 2).
101 However, before extending use of alkali-activated binders in construction material it is necessary to
102 solve some critical issue related to autogenous and drying shrinkage, considerably higher than that of
103 OPC. Finally, the durability of AAS cements is a subject of strong discussion among researchers due
104 to contradictory results reported in scientific literature (Bernal and Provis, 2014; da Costa et al., 2016;
105 Maté, 2014; Nematollahi et al., 2017; Pacheco-Torgal et al., 2012; Provis et al., 2015).

106 **2.4 The use of calcium sulphoaluminate cement**

107 The production of calcium sulfoaluminate-based binders requires a lower consumption of primary
108 energy (Tab. 1) deriving from both lower kiln temperature (1250-1300°C vs 1450°C) and grinding
109 of the lower hardness calcium sulfoaluminate clinker (Maté, 2014). Consequently, the production of
110 sulfoaluminate cement is also characterized by lower CO₂ emissions, estimated at about 25% less
111 than that of Portland cement clinker (Tab. 1 – Fig. 4). Currently, due to the high cost of raw materials
112 (bauxite, limestone and calcium sulfate), industrial by-products or waste materials (da Costa et al.,
113 2016; El-Alfi and Gado, 2016) such as fly ash, phosphogypsum, blast furnace slag, aluminium
114 anodizing sludge and marble sludge have been analyzed to manufacture calcium sulphoaluminate-
115 based clinker. However, since CSA is actually used in combination with gypsum and Portland
116 cement, the reduction of GWP and GER is about 20% and 25% respectively compared to OPC-based
117 concrete (Fig. 5). In order to reduce the environmental impact of CSA-based mixtures, the
118 replacement of Portland cement with SCMs allows to reduce both GWP and GER by 60% and 65%
119 relative to CEM I-based mortars, respectively (Fig. 5). The total replacement of OPC with FA or S
120 and hydrated lime, however, leads to a sharp reduction in compressive strength at early and later ages
121 of about 30% (Coppola et al., 2018e). Although the compressive strength of SCM-based mortars and
122 concretes is lower relative to the reference mixtures containing OPC (Coppola et al., 2018g), the more
123 stable behavior evidenced by these Portland cement-free materials makes them suitable for “cosmetic
124 repair” of existing reinforced concrete structures, where shrinkage is the main design parameter (Fig.
125 6).

2.5 The reduction in consumption of not renewable natural resources

126
127 The problem of environmental sustainability cannot be addressed solely on the basis of primary
128 energy consumption and the amount of CO₂ emitted into the atmosphere. For example, the production
129 of aggregates for concrete requires a very low consumption of primary energy (Tab. 1), about 50
130 times lower than that for the production of cement. Moreover, CO₂ emission are even almost three
131 orders of magnitude lower. On the basis of the GER and GWP it should be concluded that the use of
132 aggregates for the production of concrete is an eco-friendly activity. In reality, the production of
133 aggregates must be considered an activity that does not respect the environment as it determines a
134 consistent consumption of non-renewable resources. Therefore, we can state that among the
135 principles of sustainability in the construction sector, reducing the consumption of sand and gravel is
136 one of the basic fundamentals from which one cannot ignore. The reduction in the consumption of
137 natural aggregates can be pursued through different approaches, all, however, aimed at recovering
138 wastes (the third step of “3R Green Strategy”) from various sources (plastic bottles, glass, tires,
139 crushed asphalt, automotive shredders, foundry sands, biomass ashes, aggregates arising from
140 demolition of existing concrete structures, fresh concrete in excess returned with truck mixers and
141 washing water in ready-mix concrete plants, etc). Waste management is one of the most important
142 topics of the Green Economy and has emerged as a main research issue because, every year, only
143 about 40% of the total waste produced is recycled (Talamo and Migliore, 2017). However, a
144 consistent increase in waste recycling can be achieved only if there is a shift from the “culture” of
145 “not more than” to that of “not less than.” In fact, one of the main reasons limiting the use of waste
146 materials in concrete production is the perception that it leads to low quality structures. This
147 perception is perpetuated by standards and norms since that limit (“culture of not more than”) the
148 percentage of recycled materials, affirming indirectly that waste materials represent a poor ingredient
149 compared to natural aggregates. This approach has to be changed through regulations that specifically
150 incentivize the use of waste materials in concrete production (bonus or credit in construction tenders)
151 and increasing the taxation for disposal in landfills accompanied by strong penalties for non-

152 compliance. Adopting the approach of “at least – not less than”, if someone wants to use an eco-
153 friendly material, he has to introduce a minimum percentage of waste because the concrete can be
154 embellished of the “eco-friendly” title. Notwithstanding, obviously, the rheological, elasto-
155 mechanical and durability performances for the mixture in relation to the intended use and to the
156 environmental exposure class in which the concrete structure falls.

157 Reduction in the consumption of natural resources can also be achieved by a general increase in
158 durability of structures in order to reduce resources for maintenance and refurbishments since repair
159 materials – containing high percentage of both cement and organic polymers - have a strong impact
160 from the environmental point of view. The options that can be undertaken to achieve this goal are
161 many, but all aimed at preventing the phenomena of degradation and premature deterioration of both
162 reinforcements and concrete, such as optimizing the design of the structures to attain higher
163 robustness (Coppola et al., 2018d, 2017, 2016), carefully choosing ingredients and mixture
164 composition (Coppola et al., 2015; Ponikiewski and Gołaszewski, 2013).

165 **3. A PROPOSAL FOR A NEW EMPATHETIC ADDED SUSTAINABILITY INDEX** 166 **(EASI)**

167 Since the 21st century, the concept of sustainability in the cement and concrete industry has been
168 discussed. Damtoft *et al.* (J.S. Damtoft et al., 2008) support that sustainability in this sector can be
169 achieved by reducing greenhouse gas emissions and energy consumption in clinker production,
170 favoring the use of cements with a low clinker factor, using self-compacting concrete or ultra-high-
171 performance cement-based materials. In addition Schneider *et al.* (Schneider et al., 2011) added that
172 the key factors for realizing affordable and durable buildings and infrastructures are education and
173 R&D. Gartner and MacPhee (Gartner and MacPhee, 2011) affirmed that it is very difficult to estimate
174 the environmental damage that the concrete industry may cause in financial terms, because at the
175 moment is very difficult put a price on emitted GHGs. Also for this reason, the concept of sustainable
176 development in the concrete industry is problematic and, currently, there are no holistic models
177 capable of assessing the environmental footprint of cement-based materials. Finally, in a recent

178 review by Gartner and Hirao (Gartner and Hirao, 2015) the authors support that the sustainability is
179 a very complex subject, because there is an enormous range of possible concrete compositions
180 potentially available mixing binders, aggregates, water and admixtures.

181 In the scientific literature several methods for assessing the environmental impact of mortars and
182 concretes can be found. The sustainability indicators can be divided into two different categories:
183 first and second generation indexes. The first ones are very simple and the compressive strength is
184 considered as the main performance parameter for structural concrete. Damineli *et al.* (Damineli et
185 al., 2010) proposed two simplified indexes to evaluate the environmental footprint of mortars and
186 concretes. The first one is the binder intensity (bi) which measures the total amount of binder
187 necessary to deliver one unit of a given performance indicator e.g. 1 MPa of strength.

$$bi = \frac{b}{p} \quad (1)$$

188 Where b is the total consumption of binder materials (kg/m^3) and p is the performance requirement.
189 The second indicator is the CO_2 intensity (ci) defined as the amount of carbon dioxide emitted to
190 deliver one unit of performance.

$$ci = \frac{c}{p} \quad (2)$$

191 Where c is the total CO_2 (kg/m^3) emitted to produce and transport all concrete raw ingredients.
192 Indexes of second generation take into account different parameters, but they are not able to express
193 the sustainability in its complexity. For example, Gettu (Gettu et al., 2018) introduced the A-index
194 (so called Apathy Index) that considers both the environmental impact and the service life. However,
195 no performance parameter is taken into account.

196 Muller *et al.* (Müller et al., 2018) proposed the Building Material Sustainability Potential (BMSP),
197 that evaluates the sustainability of a concrete in relation to its mechanical performance and durability.

$$BMSP = \frac{\text{Service life} \cdot \text{Performance}}{\text{GHG emissions}} \quad \left[\frac{\text{MPa} \cdot \text{y}}{\text{kgCO}_2} \right] \quad (3)$$

198 This index is the most complex and well-structured reported in the literature. The equation addressing
199 the three basic pillars of sustainability, i.e. environmental aspects (by introducing the GHG emissions)
200 as well as socioeconomic aspects (contained in the service life and performance parameters). The
201 service life design process is characterized by assessing the link between the alteration – i.e. ageing
202 and often deterioration – of the material on one hand and the varying exposures on the other. As
203 socioeconomic aspects, however, are extremely difficult or even impossible to evaluate during the
204 concrete development process. Nevertheless, the denominator overlooks important issues such as the
205 energy requirements and the natural resources consumption.

206 Starting from the BMSP, a new “**Empathetic Added Sustainability Index (EASI)**” is here proposed
207 taking into account both the environmental impact of mortars and concretes but also the durability
208 performance and the engineering properties required depending on the specific application
209 (reinforced concrete elements, plasters, material for repair of existing structures, etc.). In other words,
210 a new EASI states on the fact that for mixtures based on both alternative cements to OPC and recycled
211 aggregates replacing natural sand and gravel, there is a need for extensive testing to establish
212 engineering design properties beyond sustainability parameters. All of the design properties
213 commonly used for traditional Portland cement concrete must be verified including compressive and
214 tensile strength, bond to reinforcing steel, shrinkage and creep, shear properties, durability
215 performance, etc, taking into account that life-safety provisions will always take precedence over
216 sustainability issues.

217 The Empathetic Added Sustainability Index (EASI) is the answer to these needs since it takes into
218 consideration design engineering performance, durability properties, life-safety provisions and
219 sustainability issues. EASI is expressed as follows:

$$EASI = \frac{3 \cdot \prod_1^n Performance \cdot \prod_1^n Durability}{\sum_1^n Environmental\ impact} \quad (4)$$

220 Where:

221 - The “*Environmental impact*” is considered the main factor related to the eco-compatibility
222 of the materials:

$$\sum_1^n Environmental\ impact = GER + GWP + NRMC \quad (5)$$

223 It takes into account:

- 224 i) the CO₂ emission estimated using the Global Warming Potential (**GWP**) parameter,
225 ii) the production energy calculated through the Gross Energy Requirement (**GER**) parameter,
226 iii) the consumption of non-renewable natural resources, including natural aggregates and
227 drinking water, estimated using the Natural Raw Materials Consumption (**NRMC**) parameter;

228 - “*Performance*”:

$$\prod_1^n Performance \quad (6)$$

229 are selected depending on the specific application of the construction material. Table 2 shows
230 a non-exhaustive example list of the engineering properties considered under “Performance”;

231 - “*Durability*”:

$$\prod_1^n Durability \quad (7)$$

232 takes into account properties required for the construction material depending on
233 environmental exposure and potential deterioration of both mortars/concretes and steel
234 reinforcements. The Table 3 shows a non-exhaustive example list of durability properties
235 considered.

236 According to EASI, three basic approaches to a sustainable use of concrete exist:

- 237 i) the optimization of mixtures composition regarding its environmental impact while
238 maintaining an equal or better performance and service life,
239 ii) the improvement of mortar’s and concrete’s performance at equal environmental impact and
240 service life,

241 iii) the optimization of service life of buildings and infrastructures at equal impact and
242 performance.

243 A combination of the above named approaches appears reasonable. For example, for a mixture to be
244 used in construction of a reinforced concrete element exposed to the potential attack of chloride-rich
245 solutions, EASI can be calculated as:

$$EASI_{Cl} = \frac{3 \cdot Rc_{28} \cdot 1/C_{Cl}}{NRMC + GER + GWP} \quad (8)$$

246 Where Rc_{28} is the 28-day compressive strength and C_{Cl} is the thickness of concrete penetrated by
247 chloride in 50 years of service life (depending on both porosity and chloride binding capacity of the
248 specific binder used for its production). All the factors are normalized respect to a reference Portland
249 cement-based concrete.

250 The same for a concrete to be used for a reinforced element exposed to air to the potential corrosion
251 promoted by carbon dioxide, the K_{CO_2} parameter is used instead of C_{Cl} according to the following
252 equation:

$$EASI_{CO_2} = \frac{3 \cdot Rc_{28} \cdot 1/K_{CO_2}}{NRMC + GER + GWP} \quad (9)$$

253 Starting from data reported in the scientific literature, it is possible, for instance, to calculate EASI
254 (Table 4) for:

- 255 i) a traditional OPC concrete (OPC),
- 256 ii) a high volume fly ash concrete (HVFA),
- 257 iii) an alkali-activated slag concrete (AAS),
- 258 iv) a CSA-based ternary binder concrete (CSA), and
- 259 v) an OPC concrete manufactured with EAF slag aggregates instead of natural aggregates
260 (EAF).

261 The analysis of EASI values shows how durability strongly influences the sustainability of concretes
262 and mortars. In fact, in chloride-rich environments, the AAS and HVFA mixtures shows a

263 sustainability index higher than that of all other investigated mixtures. On the contrary, CSA-based
264 mixtures show a EASI lower than that of OPC concrete due to its relatively high chloride apparent
265 coefficient diffusion. Furthermore, for structures exposed to CO₂, the most sustainable solution
266 among those shown in Table 4 seems to be based on the use of HVFA concrete (Fig. 7).
267 Conversely, for a thermal plaster applied on the outside surface of a stone wall exposed to freeze and
268 thaw cycles, the EASI can be calculated as:

$$EASI = \frac{1/K \cdot 1/\sigma_{cs} \cdot f_t \cdot 1/N_{50\%}}{NRMC + GER + GWP} \quad (10)$$

269 Where K is the thermal conductivity of plaster, $\sigma_{cs} = E \cdot \epsilon_{cs}$ is the tensile stress induced by restrained
270 shrinkage, f_t is the tensile strength and $N_{50\%}$ is the number of cycles needed to reduce by half the
271 tensile strength of plaster subjected to freeze/thaw cycles. All the factors are normalized respect to a
272 reference NHL-based render.

273 Starting from the data reported in the previous chapters and in the scientific literature, it is possible
274 to calculate EASI (Table 5) for:

- 275 i) a traditional plaster manufactured with natural hydraulic lime (NHL),
- 276 ii) a traditional render based on hydrated lime (HL),
- 277 iii) a lightweight alkali-activated slag mortars (LW-AAS), and
- 278 iv) a lightweight gypsum-hydrated lime plaster (LW-GY/HL) as reported in Table 5.

279 Results indicated that the lightweight plaster based on alkali-activated slag has an EASI about 7 times
280 higher than that of normal weight HL mixtures due to the better durability in cold climate and the
281 lower thermal conductivity that ensure a better thermal insulation (Fig. 8). Moreover, the total
282 substitution of binder based on natural raw materials such as NHL and gypsum with industrial by-
283 products such as GGBFS determine a sharp reduction of NRMC and, subsequently, an increase in
284 sustainability index.

285 4. CONCLUSIONS

286 In conclusion, the main contributions of current investigation are summarized as:

- 287 - In the scientific literature, several sustainability indexes are available. Nevertheless, these
288 indexes are not exhaustive due to the complexity of the topic.
- 289 - A new Empathetic Added Sustainability Index (EASI) was developed taking into account
290 both the environmental impact of mortars and concretes (GER, GWP, NRMC) but also the
291 durability and the engineering performance required as a function of the environmental
292 exposure.
- 293 - A new EASI states on the fact that for mixtures based on both alternative binders to OPC and
294 recycled aggregates there is a need for alternative testing to establish engineering properties
295 beyond sustainability parameters.
- 296 - EASI takes into account all the design properties commonly used for traditional Portland
297 cement concrete including compressive and tensile strength, elastic modulus, bond, shrinkage
298 and creep shear properties and durability performance.
- 299 - EASI affirms that life-safety provisions of construction materials will always take precedence
300 over sustainability issues.
- 301 - EASI demonstrated that AAS and HVFA reinforced concretes are characterized by the lower
302 environmental impact in chloride-rich environments. On the other hand, in CO₂-rich
303 environments, the best solution in terms of sustainability is represented by the HVFA
304 concretes.
- 305 - For a thermal plaster exposed to freeze and thaw cycles, EASI clearly showed that AAS
306 lightweight plaster is the most appropriate solution.

307

- 309 Ann, K.Y., Cho, C.-G., 2014. Corrosion Resistance of Calcium Aluminate Cement Concrete
 310 Exposed to a Chloride Environment. *Mater. (Basel, Switzerland)* 7, 887–898.
 311 <https://doi.org/10.3390/ma7020887>
- 312 Aranda Usón, A., López-Sabirón, A.M., Ferreira, G., Llera Sastresa, E., 2013. Uses of alternative
 313 fuels and raw materials in the cement industry as sustainable waste management options.
 314 *Renew. Sustain. Energy Rev.* 23, 242–260.
- 315 Barcelo, L., Kline, J., Walenta, G., Gartner, E., 2014. Cement and carbon emissions. *Mater. Struct.*
 316 47, 1055–1065. <https://doi.org/10.1617/s11527-013-0114-5>
- 317 Bernal, S.A., Provis, J.L., 2014. Durability of alkali-activated materials: Progress and perspectives.
 318 *J. Am. Ceram. Soc.* 97, 997–1008. <https://doi.org/10.1111/jace.12831>
- 319 Burak Uzal, P. Kumar Mehta, L.T., n.d. High-Volume Natural Pozzolan Concrete for Structural
 320 Applications. *Mater. J.* 104. <https://doi.org/10.14359/18910>
- 321 Černý, R., Kunca, A., Tydlitát, V., Drchalová, J., Rovnaníková, P., 2006. Effect of pozzolanic
 322 admixtures on mechanical, thermal and hygric properties of lime plasters. *Constr. Build.*
 323 *Mater.* 20, 849–857. <https://doi.org/10.1016/j.conbuildmat.2005.07.002>
- 324 Chen, C., Habert, G., Bouzidi, Y., Jullien, A., 2010. Environmental impact of cement production:
 325 detail of the different processes and cement plant variability evaluation. *J. Clean. Prod.* 18,
 326 478–485. <https://doi.org/10.1016/j.jclepro.2009.12.014>
- 327 Coppola, L., Coffetti, D., Crotti, E., 2018a. Plain and Ultrafine Fly Ashes Mortars for
 328 Environmentally Friendly Construction Materials. *Sustainability* 10, 874.
 329 <https://doi.org/10.3390/su10030874>
- 330 Coppola, L., Coffetti, D., Crotti, E., 2018b. Pre-packed alkali activated cement-free mortars for
 331 repair of existing masonry buildings and concrete structures. *Constr. Build. Mater.* 173, 111–
 332 117. <https://doi.org/10.1016/j.conbuildmat.2018.04.034>
- 333 Coppola, L., Coffetti, D., Crotti, E., 2018c. Use of tartaric acid for the production of sustainable
 334 Portland-free CSA-based mortars. *Constr. Build. Mater.* 171, 243–249.
 335 <https://doi.org/10.1016/j.conbuildmat.2018.03.137>
- 336 Coppola, L., Coffetti, D., Crotti, E., 2018d. Innovative carboxylic acid waterproofing admixture for
 337 self-sealing watertight concretes. *Constr. Build. Mater.* 171, 817–824.
 338 <https://doi.org/10.1016/j.conbuildmat.2018.03.201>
- 339 Coppola, L., Coffetti, D., Crotti, E., Pastore, T., 2018e. CSA-based Portland-free binders to
 340 manufacture sustainable concretes for jointless slabs on ground. *Constr. Build. Mater.* 187,
 341 691–698. <https://doi.org/10.1016/j.conbuildmat.2018.07.221>
- 342 Coppola, L., Lorenzi, S., Garlati, S., Kara, P., 2016. The rheological and mechanical performances
 343 of concrete manufactured with blended admixtures based on phosphonates, *Key Engineering*
 344 *Materials*.
- 345 Coppola, L., Lorenzi, S., Kara, P., Garlati, S., 2017. Performance and Compatibility of
 346 Phosphonate-Based Superplasticizers for Concrete. *Buildings* 7, 62.
- 347 Coppola, L., Lorenzi, S., Pellegrini, S., 2015. Rheological and mechanical performances of concrete
 348 manufactured by using washing water of concrete mixing transport trucks. *ACI Spec. Publ.*
 349 32.1-32.12.
- 350 da Costa, E.B., Rodríguez, E.D., Bernal, S.A., Provis, J.L., Gobbo, L.A., Kirchheim, A.P., 2016.
 351 Production and hydration of calcium sulfoaluminate-belite cements derived from aluminium
 352 anodising sludge. *Constr. Build. Mater.* 122, 373–383.
 353 <https://doi.org/10.1016/j.conbuildmat.2016.06.022>
- 354 Damineli, B.L., Kemeid, F.M., Aguiar, P.S., John, V.M., 2010. Measuring the eco-efficiency of
 355 cement use. *Cem. Concr. Compos.* 32, 555–562.
 356 <https://doi.org/10.1016/j.cemconcomp.2010.07.009>

- 357 Damtoft, J.S., Lukasik, J., Herfort, D., Sorrentino, D., Gartner, E.M., 2008. Sustainable
358 development and climate change initiatives. *Cem. Concr. Res.* 38, 115–127.
359 <https://doi.org/10.1016/j.cemconres.2007.09.008>
- 360 Damtoft, J.S., Lukasik, J., Herfort, D., Sorrentino, D., Gartner, E.M., 2008. Sustainable
361 development and climate change initiatives. *Cem. Concr. Res.* 38, 115–127.
362 <https://doi.org/10.1016/J.CEMCONRES.2007.09.008>
- 363 Duxson, P., Provis, J.L., Lukey, G.C., van Deventer, J.S.J., 2007. The role of inorganic polymer
364 technology in the development of ‘green concrete.’ *Cem. Concr. Res.* 37, 1590–1597.
365 <https://doi.org/10.1016/J.CEMCONRES.2007.08.018>
- 366 El-Alfi, E.A., Gado, R.A., 2016. Preparation of calcium sulfoaluminate-belite cement from marble
367 sludge waste. *Constr. Build. Mater.* 113, 764–772.
368 <https://doi.org/10.1016/J.CONBUILDMAT.2016.03.103>
- 369 Faleschini, F., Alejandro Fernández-Ruíz, M., Zanini, M.A., Brunelli, K., Pellegrino, C.,
370 Hernández-Montes, E., 2015. High performance concrete with electric arc furnace slag as
371 aggregate: Mechanical and durability properties. *Constr. Build. Mater.* 101, 113–121.
372 <https://doi.org/10.1016/J.CONBUILDMAT.2015.10.022>
- 373 Gartner, E., Hirao, H., 2015. A review of alternative approaches to the reduction of CO₂ emissions
374 associated with the manufacture of the binder phase in concrete. *Cem. Concr. Res.* 78, 126–
375 142. <https://doi.org/10.1016/j.cemconres.2015.04.012>
- 376 Gartner, E.M., MacPhee, D.E., 2011. A physico-chemical basis for novel cementitious binders.
377 *Cem. Concr. Res.* 41, 736–749.
- 378 Gettu, R., Pillai, R.G., Meena, J., Basavaraj, A.S., Santhanam, M., Dhanya, B.S., 2018.
379 Considerations of Sustainability in the Mixture Proportioning of Concrete for Strength and
380 Durability. *Spec. Publ.* 326, 5.1-5.10.
- 381 Global Fly Ash Market 2024, 2016, n.d.
- 382 Izaguirre, A., Lanas, J., Álvarez, J.I., 2009. Cement and Concrete Research Effect of water-
383 repellent admixtures on the behaviour of aerial lime-based mortars. *Cem. Concr. Res.* 39,
384 1095–1104. <https://doi.org/10.1016/j.cemconres.2009.07.026>
- 385 Lamuta, C., Candamano, S., Crea, F., Pagnotta, L., 2016. Direct piezoelectric effect in
386 geopolymeric mortars. *Mater. Des.* 107, 57–64.
- 387 Maddalena, R., Roberts, J.J., Hamilton, A., 2018. Can Portland cement be replaced by low-carbon
388 alternative materials? A study on the thermal properties and carbon emissions of innovative
389 cements. *J. Clean. Prod.* 186, 933–942. <https://doi.org/10.1016/J.JCLEPRO.2018.02.138>
- 390 Maté, M.G., 2014. “ Processing and characterisation of calcium sulphoaluminate (CSA) eco-
391 cements with tailored performances .”
- 392 Messina, F., Ferone, C., Colangelo, F., Roviello, G., Cioffi, R., 2018. Alkali activated waste fly ash
393 as sustainable composite: Influence of curing and pozzolanic admixtures on the early-age
394 physico-mechanical properties and residual strength after exposure at elevated temperature.
395 *Compos. Part B Eng.* 132, 161–169. <https://doi.org/10.1016/j.compositesb.2017.08.012>
- 396 Mobili, A., Belli, A., Giosuè, C., Bellezze, T., Tittarelli, F., 2016. Metakaolin and fly ash alkali-
397 activated mortars compared with cementitious mortars at the same strength class. *Cem. Concr.*
398 *Res.* 88, 198–210.
- 399 Moffatt, E.G., Thomas, M.D.A., Fahim, A., 2017. Performance of high-volume fly ash concrete in
400 marine environment. *Cem. Concr. Res.* 102, 127–135.
401 <https://doi.org/10.1016/j.cemconres.2017.09.008>
- 402 Müller, H.S., Haist, M., Vogel, M., Moffatt, J.S., 2018. Design Approach and Properties of a New
403 Generation of Sustainable Structural Concretes. *Spec. Publ.* 326, 2.1-2.16.
- 404 Nematollahi, B., Sanjayan, J., Qiu, J., Yang, E.H., 2017. Micromechanics-based investigation of a
405 sustainable ambient temperature cured one-part strain hardening geopolymer composite.
406 *Constr. Build. Mater.* 131, 552–563. <https://doi.org/10.1016/j.conbuildmat.2016.11.117>
- 407 Neville, A.M., 1995. Properties of concrete. Longman London.

408 Özbay, E., Erdemir, M., Durmuş, H.I., 2016. Utilization and efficiency of ground granulated blast
409 furnace slag on concrete properties - A review. *Constr. Build. Mater.* 105, 423–434.

410 Pacheco-Torgal, F., Abdollahnejad, Z., Camões, A.F., Jamshidi, M., Ding, Y., 2012. Durability of
411 alkali-activated binders: A clear advantage over Portland cement or an unproven issue? *Constr.*
412 *Build. Mater.* 30, 400–405. <https://doi.org/10.1016/J.CONBUILDMAT.2011.12.017>

413 Pan, J.R., Huang, C., Kuo, J.-J., Lin, S.-H., 2008. Recycling MSWI bottom and fly ash as raw
414 materials for Portland cement. *Waste Manag.* 28, 1113–1118.
415 <https://doi.org/10.1016/J.WASMAN.2007.04.009>

416 Ponikiewski, T., Gołaszewski, J., 2013. The Rheological and Mechanical Properties of High-
417 performance Self-compacting Concrete with High-calcium Fly Ash. *Procedia Eng.* 65, 33–38.
418 <https://doi.org/10.1016/J.PROENG.2013.09.007>

419 Provis, J.L., Palomo, A., Shi, C., 2015. Advances in understanding alkali-activated materials. *Cem.*
420 *Concr. Res.* 78, 110–125.

421 Puertas, F., García-Díaz, I., Barba, A., Gazulla, M.F., Palacios, M., Gómez, M.P., Martínez-
422 Ramírez, S., 2008. Ceramic wastes as alternative raw materials for Portland cement clinker
423 production. *Cem. Concr. Compos.* 30, 798–805.
424 <https://doi.org/10.1016/J.CEMCONCOMP.2008.06.003>

425 Rahman, A., Rasul, M.G., Khan, M.M.K., Sharma, S., 2015. Recent development on the uses of
426 alternative fuels in cement manufacturing process. *Fuel* 145, 84–99.

427 Ramezaniapour, A.A., Zadeh, F.B., Zolfagharnasab, A., Ramezaniapour, A.M., 2017.
428 Mechanical properties and chloride ion penetration of alkali activated slag concrete, in: *High*
429 *Tech Concrete: Where Technology and Engineering Meet - Proceedings of the 2017 Fib*
430 *Symposium*. Springer International Publishing, Cham, pp. 2203–2212.
431 https://doi.org/10.1007/978-3-319-59471-2_252

432 Salas, D.A., Ramirez, A.D., Rodríguez, C.R., Petroche, D.M., Boero, A.J., Duque-Rivera, J., 2016.
433 Environmental impacts, life cycle assessment and potential improvement measures for cement
434 production: a literature review. *J. Clean. Prod.* 113, 114–122.
435 <https://doi.org/10.1016/J.JCLEPRO.2015.11.078>

436 Schneider, M., Romer, M., Tschudin, M., Bolio, H., 2011. Sustainable cement production-present
437 and future. *Cem. Concr. Res.* 41, 642–650.

438 SIA 2030:2010 “Recycling Beton,” 2010.

439 Talamo, C., Migliore, M., 2017. Le utilità dell’inutile : economia circolare e strategie di riciclo dei
440 rifiuti pre-consumo per il settore edilizio. Maggioli.

441 Van den Heede, P.; De Belie, N., 2010. Durability Related Functional Units for Life Assessment of
442 High-Volume Fly Ash Concrete. *Second Int. Conf. Sustain. Constr. Mater. Technol. Porc.*
443 583–594.

444 Vimmrová, A., Keppert, M., Michalko, O., Černý, R., 2014. Calcined gypsum-lime-metakaolin
445 binders: Design of optimal composition. *Cem. Concr. Compos.* 52, 91–96.
446 <https://doi.org/10.1016/j.cemconcomp.2014.05.011>

447 Zementwerke, V.D., 2014. 7th International VDZ Congress Process Technology of Cement
448 Manufacturing. Verlag Bau+Technik.

449
450

451

Table 1 - Environmental properties of binders, activators and aggregates (Source: Ecoinvent 3.0 Databased)

	GER [MJ/kg]	GWP [kgCO₂/kg]
OPC	5.50	0.98
CSA	2.70	0.74
GGBFS	0.31	1.7·10 ⁻²
Fly-ash	0.10	5.3·10 ⁻³
Sodium Metasilicate pentahydrate	10.58	1.24
Potassium hydroxide	20.50	1.94
Sodium carbonate	7.23	2.20
Aggregates	0.13	2.4·10 ⁻³

452

453

Table 2 - Performance taking into account for different applications

Application	Performance
Structural reinforced concrete elements	28-day compressive strength, elastic modulus, bond strength
Concrete for slabs on ground	Flexural and tensile strength, shrinkage, elastic modulus
Concrete for massive structures	28-day compressive strength, heat of hydration
Mortar for restoration of existing structures	Shrinkage, elastic modulus, tensile strength
Concrete for prefabricated elements	Early ages compressive strength
Plasters and renders	Shrinkage, elastic modulus, tensile strength
Thermal plasters	Shrinkage, elastic modulus, tensile strength, thermal resistance
Grouting mortar	Very early compressive strength, tensile strength, bond strength

454

455

Table 3 - Durability of concrete exposed to different environments

Exposure conditions	Durability
Reinforced concrete exposed to air	Carbonation rate
Reinforced concrete exposed to deicing salts	Chloride migration coefficient
Reinforced concrete exposed to seawater	Chloride migration coefficient, sulfate resistance
Concrete exposed to freeze/thaw cycles	Freeze/thaw resistance
Concrete exposed to acid environments	Chemical attack resistance

456

457

458

459

460

Table 4 - Mixture composition, durability and environmental parameters fo concretes

	OPC	HVFA	AAS	CSA	EAF
Reference	(Moffatt et al., 2017)	(Moffatt et al., 2017)	(Ramezani pour et al., 2017)	(Ann and Cho, 2014)	(Faleschini et al., 2015)
CEM I [kg/m ³]	347	154			400
Fly Ash [kg/m ³]		195			
GGBFS [kg/m ³]			400		
CSA [kg/m ³]				264	
C \bar{S} [kg/m ³]				66	
Na ₂ SiO ₃ [kg/m ³]			36		
KOH [kg/m ³]			24		
Water [kg/m ³]	132	123	160	132	200
Nat. aggr. [kg/m ³]	1903	1897	1790	1854	965
EAF aggr. [kg/m ³]					1190
R _{c28} [MPa]	59	52	58	52	56
NRMC [kg/m ³]	2382	2174	2010	2184	1565
GER [MJ/m ³]	2156	1113	1230	1040	2480
GWP [kg CO ₂ /m ³]	345	157	102	216	397
C _{cl} [mm]	59	32	34	131	62
EASI	1.00	2.91	3.36	0.66	1.03
K _{CO2} [m/y ^{0.5}]	0.53	0.70	1.03	1.92	0.55
EASI	1.00	1.20	1.00	0.41	1.04

Table 5 - Mixture composition, durability and environmental parameters of plasters

	NHL	HL	LW-AAS	LW-GY/HL
Reference	(Černý et al., 2006)	(Izaguirre et al., 2009)	/	(Vimmrová et al., 2014)
NHL [kg/m ³]	400			120
AL [kg/m ³]		342		
GGBFS [kg/m ³]			270	
Gypsum [kg/m ³]				250
Activators [kg/m ³]			65	
Aggregates [kg/m ³]	1200	1286	250	500
Water [kg/m ³]	300	410	155	200
Density [kg/m ³]	1660	1670	760	930
E [GPa]	0.80	1.00*	1.50	2.50
ε _{cs} [mm/m]	4.50	13.00	2.20	5.80
Tensile strength [MPa]	0.50*	0.65*	1.95	1.10*
K [W/mK]	0.73	0.60	0.35	0.20
N _{50%}	15*	12*	30*	32
NRMC [kg/m ³]	1900	2038	470	1070
GER [MJ/m ³]	1356	1706	1052	750
GWP [kg CO ₂ /m ³]	123	147	109	97
EASI	1.00	0.30	27.82	6.62

* estimated data based on the curves shown above (Neville, 1995)

467 LIST OF FIGURES

468

469 *Fig 1 - Cement and fly-ash production*

470

471 *Fig 2 - Compressive strength of slag cement-based mortars at different alkali content (Ac)*

472

473 *Fig 3 - GWP and GER parameters normalized to those of an OPC-based mortar*

474

475 *Fig 4 - Carbon dioxide emissions to produce OPC and CSA*

476

477 *Fig 5 - GWP and GER parameters normalized to those of an OPC-based concrete at equal strength*
478 *class (C30/37)*

479

480 *Fig 6 - Expansive/shrinkage behavior of CSA-based mortars and Portland-based mortars.*

481

482 *Fig 7 – Empathetic Added Sustainability index of different concretes in Cl-rich or CO₂-rich*
483 *environment*

484

485 *Fig 8 – Empathetic Added Sustainability index of different plasters*

486